

工 學 碩 士 學 位 論 文

**Research on program for determination of suitable
welding condition for the curved block**

指導教授 朴 珠 用

2000年 2月

韓國海洋大學校 大學院

造 船 工 學 科

安 大 鎬

本 論 文 安大鎬 工學碩士 學位論文 認 准 .

主 審 : 工學博士 朴 命 圭 (印)

副 審 : 工學博士 趙 孝 濟 (印)

副 審 : 工學博士 朴 珠 用 (印)

2000年 2月

韓國海洋大學校 大學院

Abstract

.....

List of Figures

List of Tables

1	1
2	 3
2.1	3
2.2	7
3	9
3.1	9
3.2	10
3.3	12
4	14
4.1	14
4.2	15
5	21
5.1	21
5.2	23
5.3	24
5.4	27

5.5	35
5.6	36
6	39
7	42
	43

**Research on program for determination
of suitable welding condition for the curved block.**

Dae-ho An

Dept. of Naval Architecture, Graduate School,
Korea Maritime University

Abstract

Welding is one of the main processes in a ship construction. Automation of welding is a key work to increase the productivity of the shipbuilding. Welding robots and special automatic welding machines are widely used at the assembly stage for plane block. However, these automatic machines are not used yet for the curved blocks because they contain very complex and continuously changed weld joints. To achieve the automatization of welding for the curved block, an highly intelligent automatic welding system is required. Getting the optimal welding parameters is an important part for the suitable use of this automatic system.

This research aims to do develop a computer program for determination of suitable welding condition for the curved block of a ship hull. In this paper the relationships between welding parameters such as current and voltage, current and deposition rate were investigated through literature survey, theoretical study and the welding experiments. The concept of the critical deposited area and suitable welding current for that area are introduced to get the sound bead at the various inclination of the joint. This area and the current are dependent on the joint inclination and their relationships could be determined by a lot of welding experiments and use of artificial neural network.

Suitable pass number and the other welding parameters could be determined by the relationships between the critical area and the welding parameters. Finally, an algorithm to determine suitable parameter values was developed on the basis of their investigations and realized into a pc program.

P

μ_0

J

I

P CO2

B

α, β 가 ,

V_{min}

V_{max}

V_D

l_w

V_S

ρ

$w(new)_{ij}$ i, j 가

$w(old)_{ij}$ i, j 가

α 가 , ($0 < \alpha < 1$)

a_i i

a_j j

o_{pj} p j

t_j j

t_{pj} p j

e_i i

List of Figures

- Fig. 2.1 Forces acting on the molten pool
- Fig. 2.2 Angle between bead and base metal
- Fig. 3.1 Relationship between welding voltage and welding current
- Fig. 3.2 Relationship between welding current, wire extension and deposition rate
- Fig. 3.3 Deposition area in fillet joint
- Fig. 4.1 Detail of welding specimen
- Fig. 4.2 Critical deposition area dependent on the inclination of joint
- Fig. 5.1 Configuration of neural network
- Fig. 5.2 Operative process of neuron
- Fig. 5.3 Activation functions
- Fig. 5.4 Learning process of neural network
- Fig. 5.5 Error backpropagation of generalized delta rule
- Fig. 5.6 Configuration of 2 neural network models
- Fig. 6.1 Flowchart for determination of the suitable welding condition for the curved block
- Fig. 6.2 Real time control of welding parameters

List of Tables

- Table 4.1 Experiment examples
- Table 5.1 Input pattern and target pattern used to learn the neural networks
- Table 5.2 Output pattern given by the learned neural networks

1

가

.

,

.

,

가

.

(船首尾)

,

가

.

,

가

가

,

.

가

.

가

.

,

가

.

가

.

.

가

가

[1,2,3].

2

2.1

(molten pool) ,
[4]. 가 (filler metal)
(base metal)가 ,
가 .
(大氣)
가 ,
(固液境界面) .
[5,6,7,8,9,10].
(不在)
가 .
Fig. 2.1 TIG
[11].

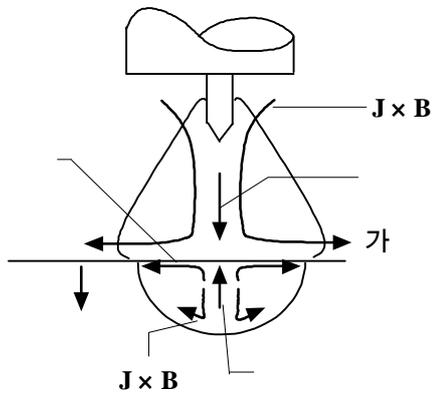


Fig. 2.1 Forces acting on the molten pool

(1) (無限長) (圓柱狀導電性流體) 가
 ,
 ,
 , 가 .
 (先端部) , TIG (2.1)
 [11].

$$p = \frac{\mu_0}{4\pi} J \cdot I \quad (2.1)$$

p : (Pa)
 μ_0 : (4 x 10⁻⁷ H/m)
 J : (A/m²)
 I : (A)

CO2

, (electrode tip)
 ,
 , (2.2)
 , 가

$$P \propto \frac{I^2}{d} \quad (2.2)$$

P : (A/m²), d : (mm)

(2)

, 가 ,
 , (2.3) [12].

$$F_m = J \times B \quad (2.3)$$

F_m : (N/m³), J : (N/m²), B : (Wb/m²)

(2.3) 가 가

, 가 ,
 가,
 , 가
 , 가
 , 가
 , 가

가 . 가 ,
가 . 가 .
(3) 2 (interface)
가 .
가 [13].
가 , 가
가 , 가
가 , 가
가 가
(4) 가
가 ,
가 Fig. 2.2
() 0°
(Undercut) 가
() 90° (Overlap)
가 , 가 ,

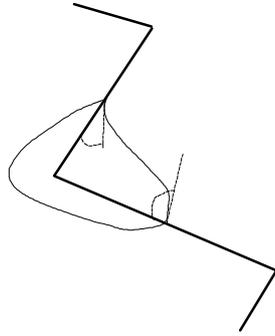


Fig. 2.2

가

: 가 ,
: 가

(5)

가 , 가

2.2

2.1

, ,
,

가 ,

가 (humping)

가 가

가
가

3

3.1

가
CO2
가
(sigmoid function)
[14].
가 가
가
가 1.4mm CO2
Fig. 3.1
(3.1), (3.2), (3.3), (3.4)
(30)
(3.1) , (3.2)
가
가 (3.3), (3.4)

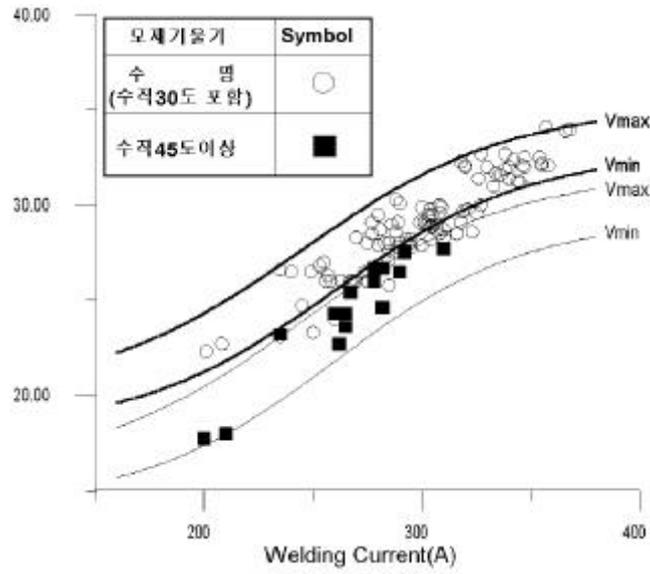


Fig. 3.1 Relationship between welding voltage and welding current

30. ,

$$V_{\max} = \frac{20.01 - 35.26}{(1 + e^{(I - 244.63)/47.964})} + 35.26 \quad (3.1)$$

$$V_{\min} = \frac{18.19 - 32.801}{(1 + e^{(I - 259.6)/44.816})} + 32.801 \quad (3.2)$$

45. ,

$$V_{\max} = \frac{16.011 - 31.72}{(1 + e^{(I - 244.63)/47.964})} + 31.72 \quad (3.3)$$

$$V_{\min} = \frac{14.19 - 29.30}{(1 + e^{(I - 259.6)/44.816})} + 29.30 \quad (3.4)$$

3.2

(deposition rate) 가

(melting rate)

가

가 ,

가 가

[15].

(3.5)

(3.5)

(3.6)

Fig. 3.2

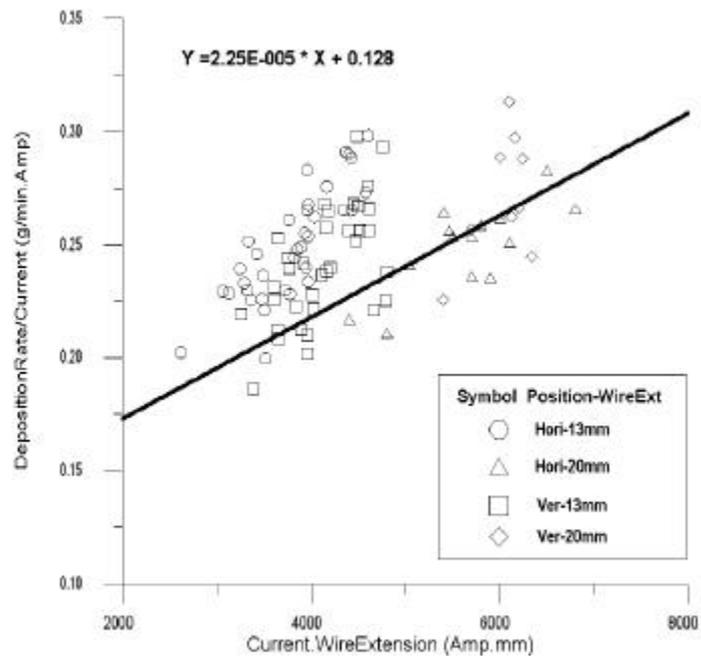


Fig. 3.2 Relationship between welding current, wire extension and deposition rate

$$V_D = b_1 \cdot I + b_2 \cdot I^2 \cdot l_w \quad (3.5)$$

$$\frac{V_D}{I} = b_1 + b_2 \cdot I \cdot l_w \quad (3.6)$$

V_D : (g/min), l_w : (mm)

$$b_1 = 0.128, \quad b_2 = 2.25 \times 10^{-5}$$

3.3

가

Fig. 3.3

가 90°

(3.7) , A1
 A2 A1 10 20%
 20% 가 (3.8) . A3
 (3.9) (3.10)
 (3.10) 가 .
 , (3.11) (3.11)
 (3.5) (3.12)
 (3.13) 가 ,
 (3.13)

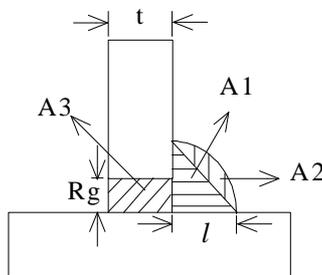


Fig. 3.3 Deposition area in fillet Joint

$$A_1 = l^2 / 2 \quad (3.7)$$

$$A_2 = 0.2 \times A_1 \quad (3.8)$$

$$A_3 = t \times R_g \quad (3.9)$$

$$A_{dep} = A_1 + A_2 + A_3 \quad (3.10)$$

$$A_{dep} = \frac{V_D \cdot 100}{V_S \cdot \rho} \quad (mm^2) \quad (3.11)$$

$$V_D = \frac{A_{dep} \cdot V_S \cdot \rho}{100} = b_1 \cdot I + b_2 \cdot I^2 \cdot l_w \quad (g/min) \quad (3.12)$$

$$V_S = \frac{(b_1 \cdot I + b_2 \cdot I^2 \cdot l_w) \cdot 100}{A_{dep} \cdot \rho} \quad (cm/min) \quad (3.13)$$

, : 7.85 g/cm³

2 Fig. 2.2 $> 0^\circ$, $< 90^\circ$.

Fig. 4.1 10mm
 $500 \times 150\text{mm}$, $500 \times 100\text{mm}$,
 0° , 15° , 30° ,
 45° , 60° , 0° , 15° , 30° , 45° , 60° , 90° .
 $30^\circ - 30^\circ$, $30^\circ - 45^\circ$, $30^\circ - 60^\circ$, $60^\circ - 30^\circ$, $60^\circ - 45^\circ$, $60^\circ - 60^\circ$

. Table. 4.1

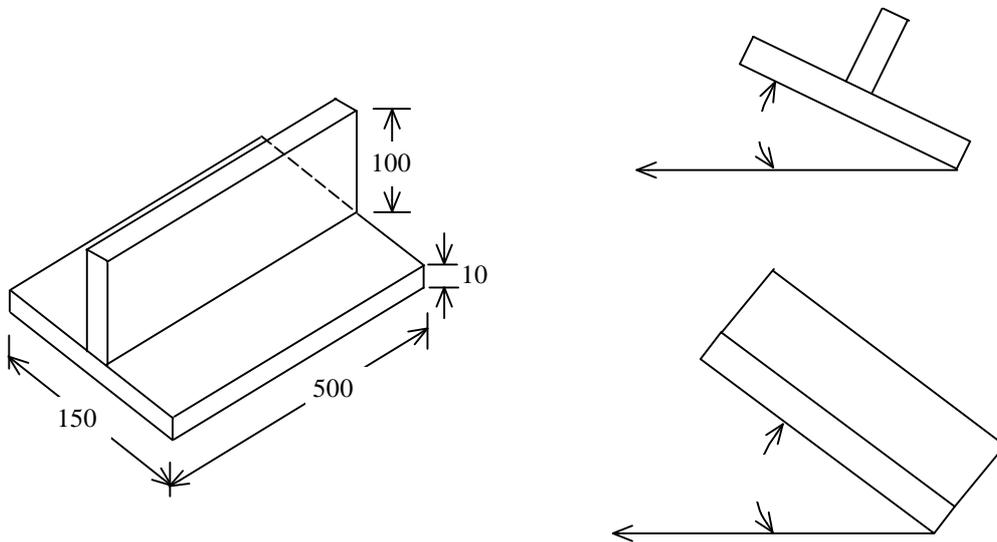


Fig. 4.1 Fig. 2.4 Detail of welding specimen

Table. 4.1 Experiment examples

1) 0°, 0°

	(A)	(V)	(cm/min)	(mm)	(mm ²)	
1	258	26.0	30	13	22.29	
2	340	31.4	60	13	16.42	

2) 15°, 0°

	(A)	(V)	(cm/min)	(mm)	(mm ²)	
3	289	29.1	30	13	26.08	
4	334	31.7	60	13	16.0	

3) 30°, 0°

	(A)	(V)	(cm/min)	(mm)	(mm ²)	
5	263	26	30	13	22.89	
6	340	32	60	13	16.5	

4) 45°, 0°

	(A)	(V)	(cm/min)	(mm)	(mm ²)	
7	269	26	30	13	23.61	
8	342	33	60	13	16.56	

5) 60°, 0°

	(A)	(V)	(cm/min)	(mm)	(mm ²)	
9	256	26	30	13	22.05	
10	323	32	60	13	15.26	

6) 15°, 0°

	(A)	(V)	(cm/min)	(mm)	(mm ²)	
11	280	27.9	31.6	13	24.96	V- Down
12	347	32	60	13	20.93	V- Down

7) 30°, 0°

	(A)	(V)	(cm/min)	(mm)	(mm ²)	
13	260	24	34.3	13	19.70	V- Down
14	285	25.2	34.3	20	27.12	V- Down

8) 45°, 0°

	(A)	(V)	(cm/min)	(mm)	(mm ²)	
15	316	26.4	70	20	15.54	V- Down
16	262	22.7	55	20	14.92	V- Down

9) 60°, 0°

	(A)	(V)	(cm/min)	(mm)	(mm ²)	
17	235	22.7	50	20	14.00	V- Down
18	200	17.7	45	20	12.34	V- Down

10) 90°, 0°

	(A)	(V)	(cm/min)	(mm)	(mm ²)	
19	278	26	73.4	20	12.21	V- Down
20	282	24.6	73.4	20	12.48	V- Down

11) 30°, 30°

	(A)	(V)	(cm/min)	(mm)	(mm ²)	
21	270	28.3	32.5	20	26.40	V- UP,
22	296	27.3	48	20	20.52	V- Down

12) 30. , 45.

	(A)	(V)	(cm/min)	(mm)	(mm ²)	
23	265	24.3	54.4	20	15.34	V- Down
24	310	27.7	64	20	16.51	V- Down

13) 30. , 60.

	(A)	(V)	(cm/min)	(mm)	(mm ²)	
25	270	26	69.5	20	12.35	V- Down
26	260	24.3	69.5	20	11.68	V- Down

14) 60. , 30.

	(A)	(V)	(cm/min)	(mm)	(mm ²)	
27	270	28.3	28.6	20	30.01	V- UP,
28	300	26.4	43.4	20	23.16	V- Down

15) 60. , 45.

	(A)	(V)	(cm/min)	(mm)	(mm ²)	
29	270	27.3	60.7	20	14.14	V- Down
30	282	26.7	60.7	20	15.09	V- Down

16) 60. , 60.

	(A)	(V)	(cm/min)	(mm)	(mm ²)	
31	268	26.5	69.5	20	12.21	V- Down
32	267	25.4	69.5	20	12.14	V- Down

가

30.

45.

가

가

Fig. 4.2

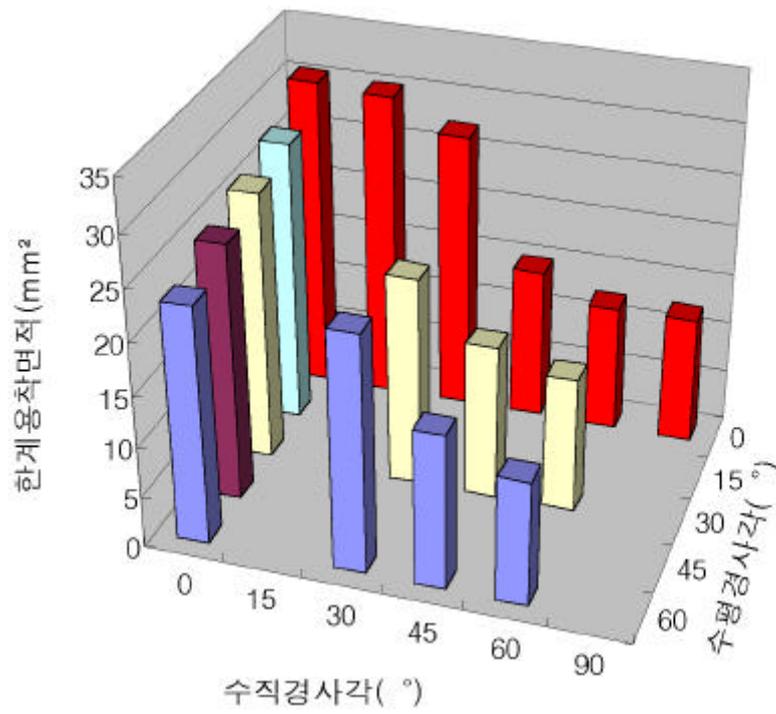


Fig. 4.2 Critical deposition area dependent on the inclination of joint

5

[18,19,20]

5.1



(fire) .
 (dendrite)
 (soma) , (axon)
 .
 가 가
 , 가 가
 가 , 가
 (activation function)[21,22]
 .

가 , 가 가
 (supervised learning) (input pattern)
 (target pattern) .

가

가 가 가 .
 가 가

가

가

5.2

가

(artificial neuron) (connection) . Fig.

5.1

가 (layer)

가

(input layer), (output layer), (hidden layer)

(plane)

가 (one layer neural network)

(multi layer network)

(fully connected network)

(partially connected network)

가 (non recurrent neural network feedforward neural network)

(recurrent neural network)

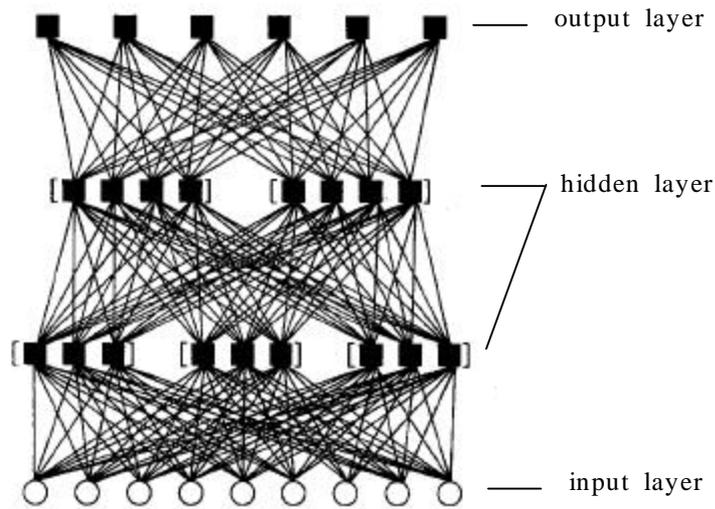


Fig. 5.1 Configuration of neural network

5.3

가

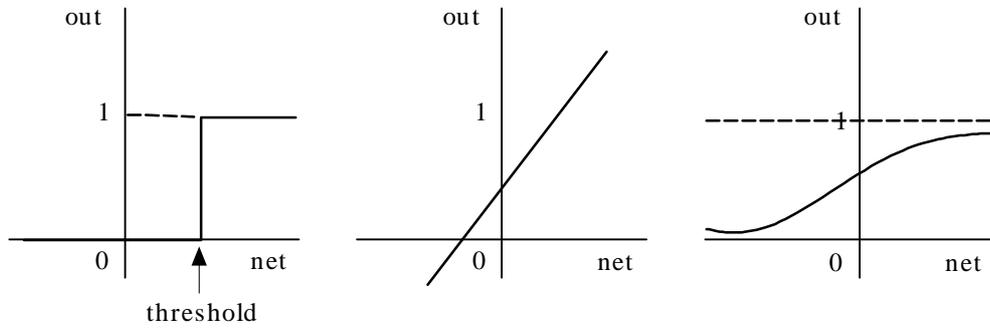
(threshold)
(fire)

Fig. 5.2

(out0, out1, ..., outn-1)

가 (w0n, wn)

(sigmoid function)



out = 1, net > threshold
 out = 0, net <= threshold

out = a · net + b
 a, b : constant

out = 1/(1+e^{-(ax-b)})
 e = 2.718282

(a) Threshold function

(b) Linear function

(c) Sigmoid function

Fig. 5.3 Activation functions

net

0 1

f(x) = ax + b

f(x) = 1 / (1 + e^{-(ax-b)})

a

b

0

a b

가

가

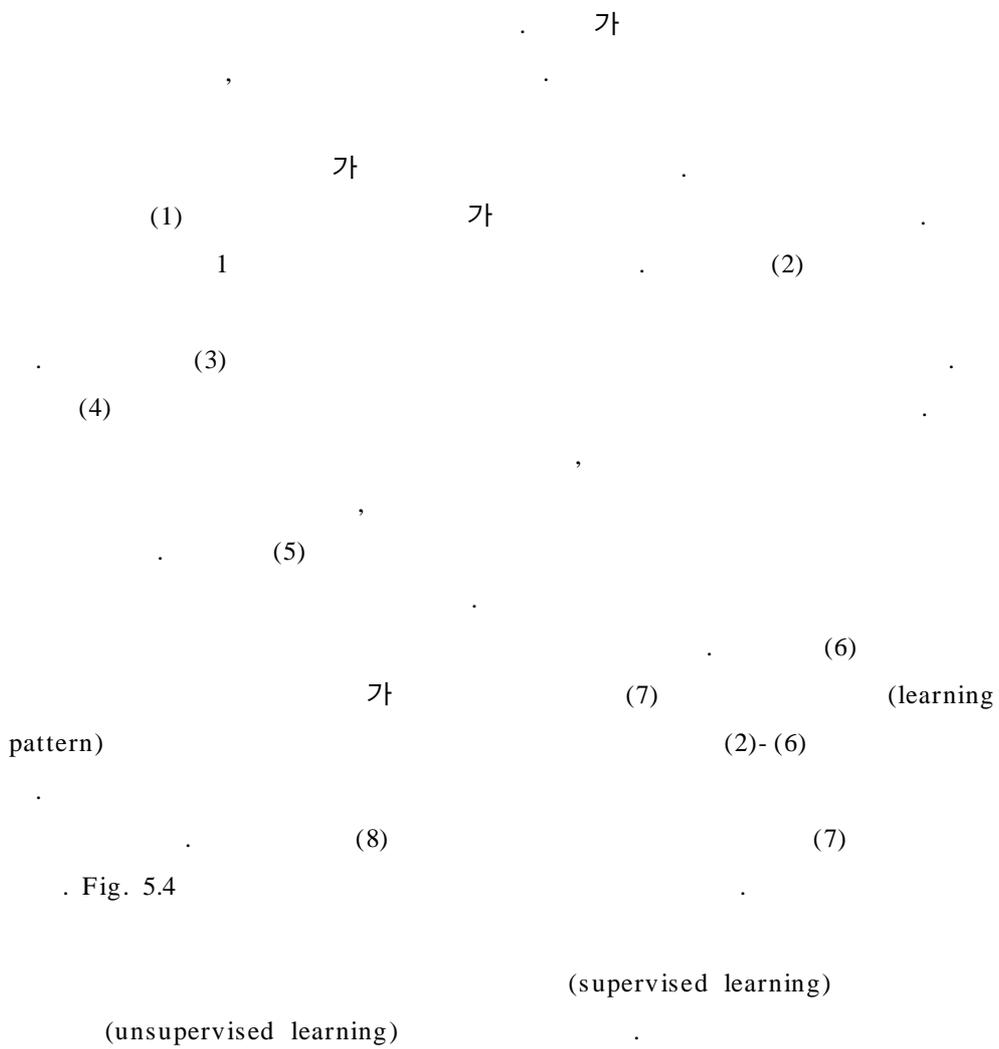
가

가 0 1

가

. Fig. 5.3

5.4



. Fig. 5.4

가

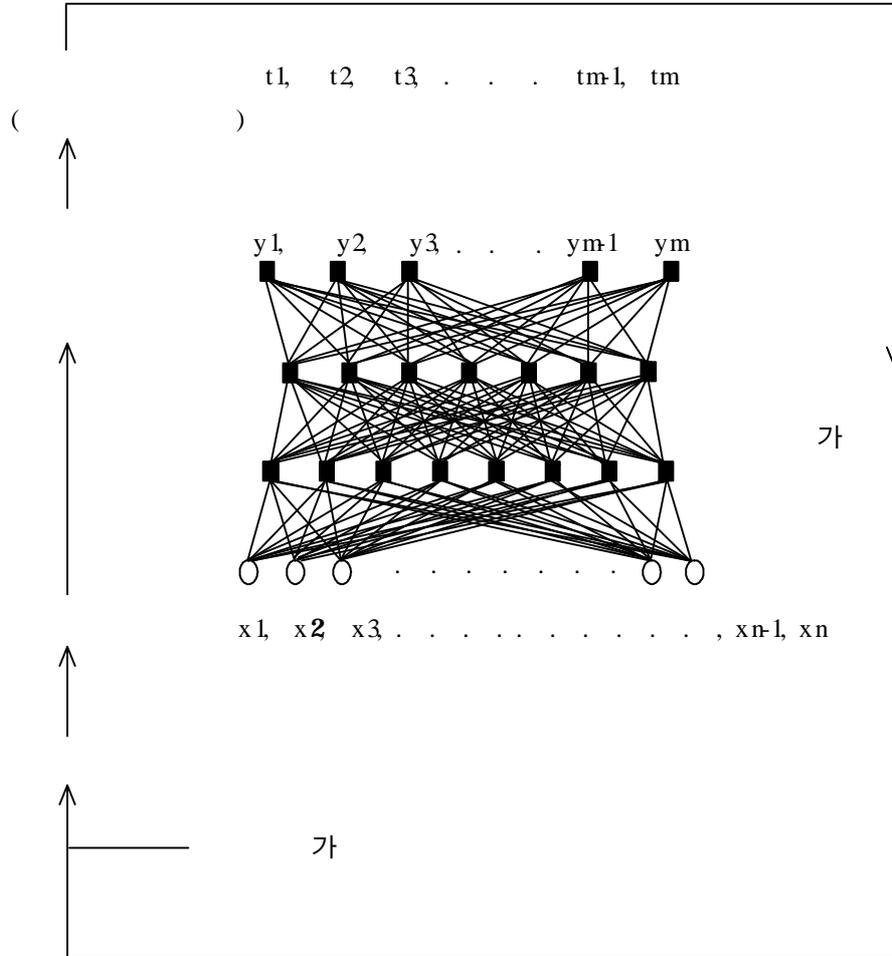


Fig. 5.4 Learning process of neural network

(pattern associator)

(Hebb's rule),

(Delta rule),

(Generalized delta rule)

가

(pattern classifier)

1949 (Donald O. Hebb)

가
 , 가 가 .”
 가 가
 (5.1)

$$w(new)_{ij} = w(old)_{ij} + a_i a_j \quad (5.1)$$

$w(new)_{ij}$: i, j 가

$w(old)_{ij}$: i, j 가

: $(0 < \alpha < 1)$

a_i : i

a_j : j

(5.1)

가 0 1
 , $w(old)_{ij}$ 가
 , $w(old)_{ij}$ 가

(1)

(2)

, (3)

가

(5.4) .

$$w(new)_{ij} = w(old)_{ij} + e_j a_i \quad (5.4)$$

j .

$$e_j = t_j - a_j \quad (5.5)$$

$w(new)_{ij}$: i, j 가
 $w(old)_{ij}$: i, j 가
 η : ($0 < \eta < 1$)
 e_j : j
 t_j : j
 a_i : i
 a_j : j

, (5.3) .

가 ,
 “ 가 가 ,
 , 가 ,
 .” .

Fig. 5.1

(hidden layer)

가

가 .

(backpropagation

$$\begin{aligned}
\delta_j & : & j \\
f'(net_j) & : & j \\
e_j & : & j \\
t_j & : & j \\
a_j & : & j
\end{aligned}$$

$$f'(net_j))$$

$$f'(x) = x(1-x) \text{ 가 } \dots \text{ 가 } ,$$

$$\text{가 } ,$$

$$\text{가 } .$$

$$\text{가 } (5.7) \quad ($$

3 4) .

$$\delta_i = f'(net_i)e_i = a_i(1-a_i)e_i \quad (5.7)$$

$$e_i = \sum_j w_{ij} \delta_j \Leftarrow$$

$$f'(net_i) = \frac{\partial f(net_i)}{\partial net_i}$$

$$= a_i(1-a_i) \Leftarrow (f'(x) = x(1-x))$$

$$w_{ij} : i \quad j \text{ 가 } \text{가}$$

$$\delta_i : i$$

$$f'(net_i) : i$$

$$e_i : i$$

$$\begin{aligned} \delta_j & : & j \\ a_i & : & i \end{aligned}$$

가
가
(5.8) 가
j j j가

$$w(new)_{ij} = w(old)_{ij} + \alpha \delta_j a_i \quad (5.8)$$

$$\begin{aligned} \delta_j & = a_j(1 - a_j)e_j \\ e_j & = t_j - a_j \Leftarrow \\ & = \sum_k w_{jk} \delta_k \Leftarrow \end{aligned}$$

$$\begin{aligned} w(new)_{ij} & : & i, j & \text{가} \\ w(old)_{ij} & : & i, j & \text{가} \\ \alpha & : & (0 < \alpha < 1) \\ \delta_j & : & j \\ a_i & : & i \\ a_j & : & j \\ e_j & : & j \end{aligned}$$

t_j : j 가

$w_{j k}$: j 가 k 가

δ_k : j 가 k

5.5

, (recall)

, (associative recall)

, 가 (competition mechanism)

가 , 가

, 가

, 가

, (1)

, (2) , (3)

, (4)

, (test pattern)

가

5.6

Fig. 5.6

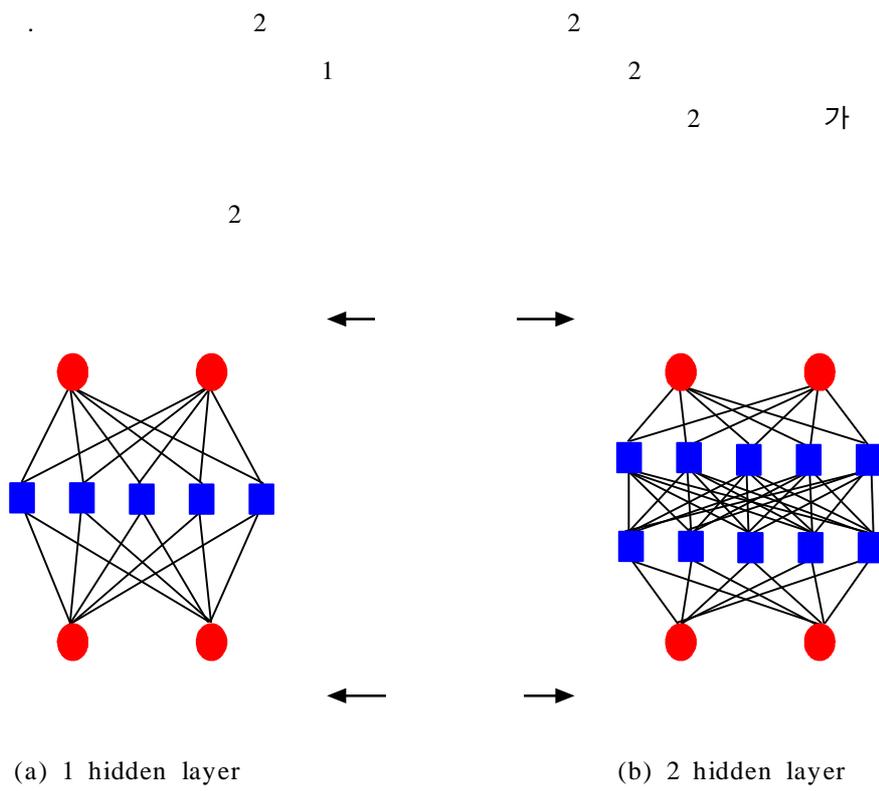


Fig. 5.6 Configuration of 2 neural network models

Table 5.1

, Table 5.2

Table 5.1 Input pattern and target pattern used to learn the neural networks

No.				
1	0	0	320	31.0
2	0	15	300	28.0
3	0	30	290	26.5
4	0	45	270	25.0
5	0	60	260	23.0
6	15	0	310	30.0
7	30	0	290	27.0
8	30	30	270	25.0
9	30	60	260	22.0
10	45	0	260	15.0
11	45	30	270	16.0
12	45	60	280	17.0
13	60	0	220	12.5
14	60	30	250	14.0
15	60	60	270	15.0
16	90	0	280	12.5

Table 5.2 Output pattern given by the learned neural networks

No.				
1	15	15	305	27.5
2	15	30	290	26.0
3	15	60	260	22.5
4	30	15	285	26.0
5	30	45	256	23.3
6	45	15	261	15.7
7	45	45	285	16.0
8	60	15	216	13.4
9	60	45	270	14.7

가

Fig. 6.1

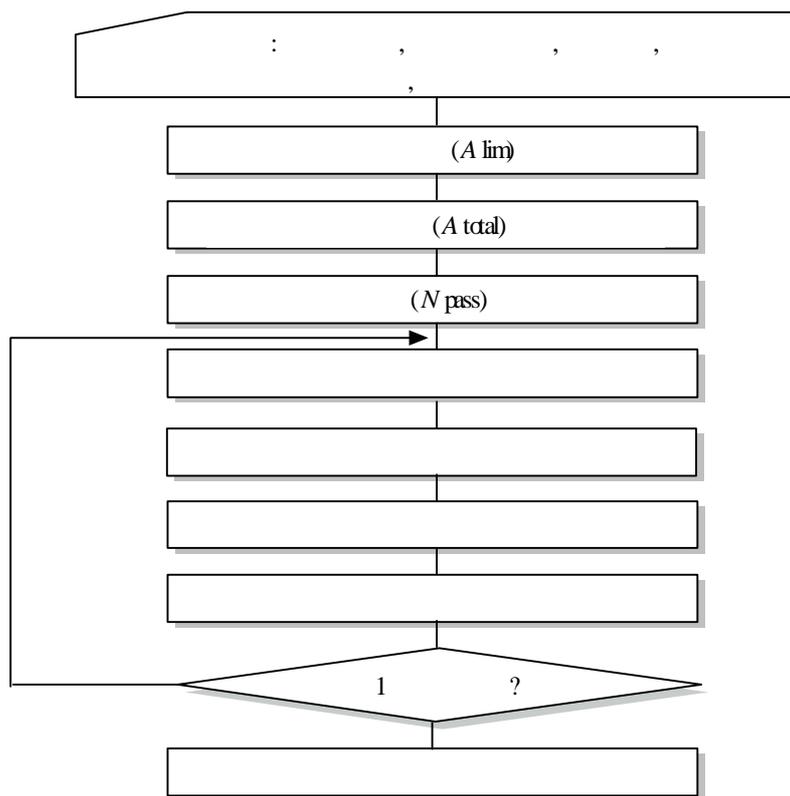


Fig. 6.1 Flowchart for determination of the suitable welding condition for the curved block.

Fig. 6.1

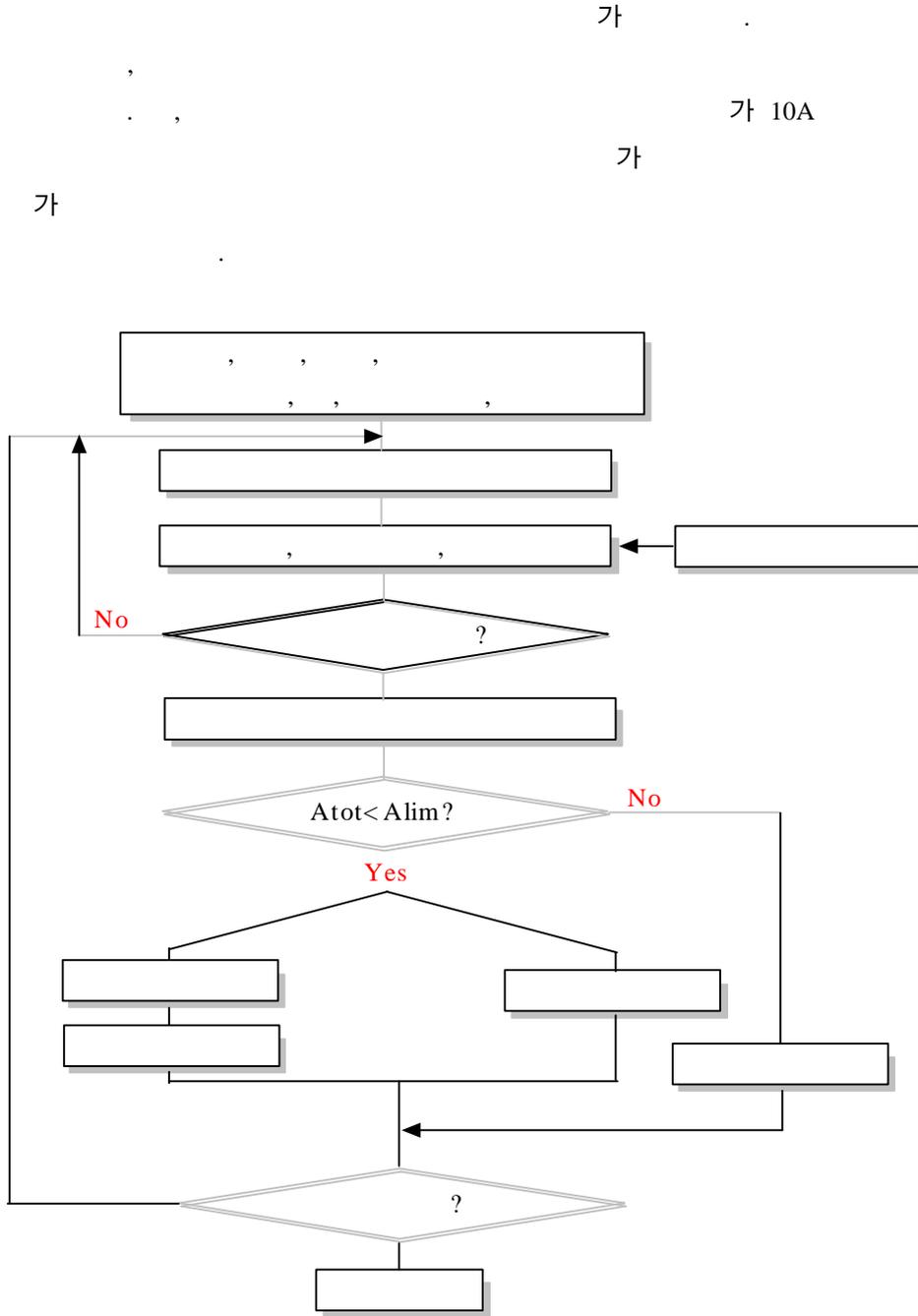


Fig. 6.2 Real time control of welding parameters

가 3mm2
, 1mm , 10°
. Fig. 6.2 .

가

,

,

7

(1) 가

(2)

(3) 2 2 1 2 2 가

(3) 30° , 30°

(4)

- [1] R. L. O'Brien, "Welding Handbook", Americal Welding Society, Vol. 2, pp 157- 233
- [2] 金銀錫, “熔接技術”, 1991
- [3] 尹斗銀, “特殊熔接工學”, 1991
- [4] 金教斗, “最新 ”, 大光書林 1998 , pp 17
- [5] K. Nishiguchi, T. Ohji and H. Matsui, "Fundamental Researchse on Bead Formation in Overlaying and Fillet Welding Processes", Japan Welding Society 45, No.1, 1976, pp 82- 87
- [6] T.Zacharia, S. A. David, J. M. Viet, “ Modeling the effect of surface active elements on weld pool fluid flow, heat transfer and geometry ”, International trends in Welding Science and Technology, ASM Proc. of the 2nd Int. Conf. on Trends in Welding Research, Gatlinburg, Tennessee, USA, 1989, pp 25- 30
- [7] W. A. Sudnik, “ Untersuchung von Schmelzschweißtechnologien anhand physikalischer mathematischer Modelle ”, Schweißen und Schneiden 43, No. 10, 1991, pp 588- 590
- [8] A. Matsunawa, “ Modeling of Heat and Fluid Flow in Arc Welding ”, International Trends in Welding Science and Technology, ASM Proc. of the 3rd Int. Conf. on Trends in Welding Research, Gatlinburg, Tennessee, USA, 1992, pp 3- 16
- [9] 西口公之, 黃地尙義, 竹林博明, "ア-ク溶接の溶融池現象に関する界面張力論

- 的解析(第1報)" 日本溶接學會誌, 第48卷, 第10 , 1979
- [10] 西口公之, 黃地尚義, 古賀宏志, “ア-ク溶接の熔融池現象に関する界面張力論的解析(第2報)” 日本溶接學會誌, 第50卷, 第5 , 1981
- [11] 社 法人 溶接學會, "溶接プロセスの物理" 溶接ア-ク物理研究委員會, 1996, pp 130, pp 48
- [12] International Institute of Welding, "The physics of welding" 1984, pp 54
- [13] Rolf H. Sabersky, Allan J. Acosta, Edward G. Hauptmann, "FLUID FLOW", Maxwellmachillan, 1992, pp 9- 11
- [14] A. Lesnewich, "Control of melting rate and metal transfer in gas shielded metal arc welding", Welding Journal 37(9), 1985, pp 343- 418
- [15] American Welding Society, "Welding Handbook", 1991 pp116- 123
- [16] I. Masumoto, T. Shinoda, J. Takano, "Program for CO2 Horizontal Fillet Welding Parameters", Japan Welding Society 48, No.11, 1979, pp 23- 27
- [17] A. Kuhne, "Ein Beitrag zur Steuerung und Regelung des automatisierten Schutzgasschweißprozesses und zur Anpassung der Schweißparameter an die jeweilige Fugengeometrie", Dissertation RWTH Aachen
- [18] , “ ”, Ohm , 1993
- [19] , “ ”, , 1997, pp 4- 15
- [20] J.Y.Park, S.H.Kim, “Expert System for Recommendation of Optimal Welding Parameter for CO2-Robotic Arc Welding in Shipbuilding”,

Taiwan International Welding Conference on Technology Advancements
and New Industrial Applications in Welding, 1998

[21] 金大洙, “ ”, , 1992

[22] 金大洙, “ ”, , 1993